National Semiconductor

December 9, 2008

LM2907/LM2917
Frequency to Voltage Converter

General Description

The LM2907, LM2917 series are monolithic frequency to voltage converters with a high gain op amp/comparator designed to operate a relay, lamp, or other load when the input frequency reaches or exceeds a selected rate. The tachometer uses a charge pump technique and offers frequency doubling for low ripple, full input protection in two versions (LM2907-8, LM2917-8) and its output swings to ground for a zero frequency input.

The op amp/comparator is fully compatible with the tachometer and has a floating transistor as its output. This feature allows either a ground or supply referred load of up to 50 mA. The collector may be taken above V_{CC} up to a maximum V_{CE} of 28V.

The two basic configurations offered include an 8-pin device with a *ground referenced tachometer* input and an internal connection between the tachometer output and the op amp non-inverting input. This version is well suited for single speed or frequency switching or fully buffered frequency to voltage conversion applications.

The more versatile configurations provide differential tachometer input and uncommitted op amp inputs. With this version the tachometer input may be floated and the op amp becomes suitable for active filter conditioning of the tachometer output.

Both of these configurations are available with an active shunt regulator connected across the power leads. The regulator clamps the supply such that stable frequency to voltage and frequency to current operations are possible with any supply voltage and a suitable resistor.

Advantages

■ Output swings to ground for zero frequency input
■ Easy to use; $V_{OUT} = f_{IN} \times V_{CC} \times R1 \times C1$

■ Only one RC network provides frequency doubling
■ Zener regulator on chip allows accurate and stable frequency to voltage or current conversion (LM2917)

Features

■ Ground referenced tachometer input interfaces directly with variable reluctance magnetic pickups
■ Op amp/comparator has floating transistor output
■ 50 mA sink or source to operate relays, solenoids, meters, or LEDs
■ Frequency doubling for low ripple
■ Tachometer has built-in hysteresis with either differential input or ground referenced input
■ Built-in zener on LM2917
■ ±0.3% linearity typical
■ Ground referenced tachometer is fully protected from damage due to swings above V_{CC} and below ground

Applications

■ Over/under speed sensing
■ Frequency to voltage conversion (tachometer)
■ Speedometers
■ Breaker point dwell meters
■ Hand-held tachometer
■ Speed governors
■ Cruise control
■ Automotive door lock control
■ Clutch control
■ Horn control
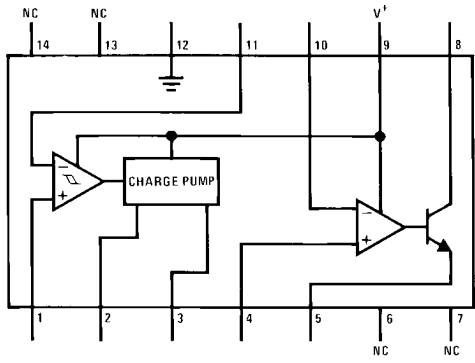■ Touch or sound switches

Connection Diagrams

Dual-In-Line and Small Outline Packages, Top Views
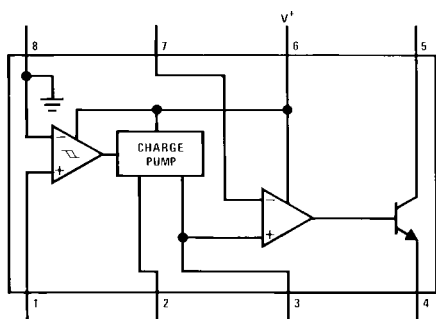
Order Number LM2907M-8 or LM2907N-8
See NS Package Number M08A or N08E
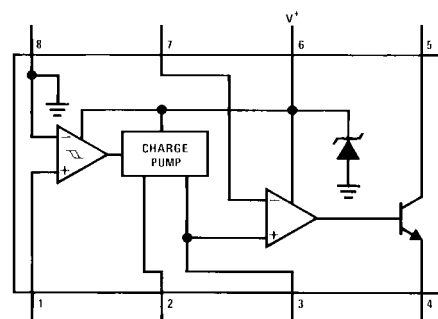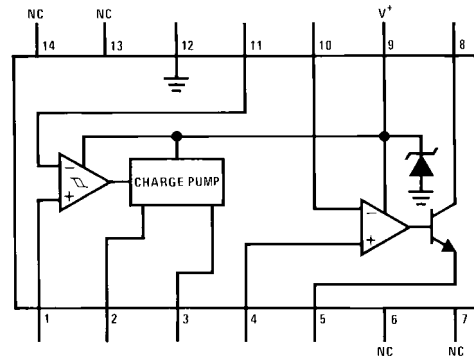

Order Number LM2917M-8 or LM2917N-8
See NS Package Number M08A or N08E

Order Number LM2907M or LM2907N
See NS Package Number M14A or N14A

794203

Order Number LM2917M or LM2917N
See NS Package Number M14A or N14A

794204

Ordering Information

Order Number	Package Type	Package Number	Package Marking	Supplied As
LM2907M-8	8-Pin SOIC Narrow	M08A	LM2907M-8	Rail of 95
LM2907MX-8	8-Pin SOIC Narrow	M08A	LM2907M-8	Reel of 2500
LM2907M	14-Pin SOIC Narrow	M14A	LM2907M	Rail of 55
LM2907MX	14-Pin SOIC Narrow	M14A	LM2907M	Reel of 2500
LM2907N-8	8-Pin Molded DIP	N08E	LM2907N-8	Rail of 40
LM2907N	14-Pin Molded DIP	N14A	LM2907N	Rail of 25
LM2917M-8	8-Pin SOIC Narrow	M08A	LM2917M-8	Rail of 95
LM2917MX-8	8-Pin SOIC Narrow	M08A	LM2917M-8	Reel of 2500
LM2917M	14-Pin SOIC Narrow	M14A	LM2917M	Rail of 55
LM2917MX	14-Pin SOIC Narrow	M14A	LM2917M	Reel of 2500
LM2917N-8	8-Pin Molded DIP	N08E	LM2917N-8	Rail of 40
LM2917N	14-Pin Molded DIP	N14A	LM2917N	Rail of 25

Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Supply Voltage	28V
Supply Current (Zener Options)	25 mA
Collector Voltage	28V
Differential Input Voltage	
Tachometer	28V
Op Amp/Comparator	28V
Input Voltage Range	
Tachometer	
LM2907-8, LM2917-8	±28V
LM2907, LM2917	0.0V to +28V

Op Amp/Comparator	0.0V to +28V
Power Dissipation	
LM2907-8, LM2917-8	1200 mW
LM2907-14, LM2917-14	1580 mW
See (Note 1)	
Operating Temperature Range	−40°C to +85°C
Storage Temperature Range	−65°C to +150°C
Soldering Information	
Dual-In-Line Package	
Soldering (10 seconds)	260°C
Small Outline Package	
Vapor Phase (60 seconds)	215°C
Infrared (15 seconds)	220°C

Electrical Characteristics

V_{CC} = 12 V_{DC}, T_A = 25°C, see test circuit

Symbol	Parameter	Conditions	Min	Typ	Max	Units
TACHOMETER						
	Input Thresholds	V_{IN} = 250 mVp-p @ 1 kHz (Note 2)	±10	±25	±40	mV
	Hysteresis	V_{IN} = 250 mVp-p @ 1 kHz (Note 2)		30		mV
	Offset Voltage	V_{IN} = 250 mVp-p @ 1 kHz (Note 2)				
	LM2907/LM2917			3.5	10	mV
	LM2907-8/LM2917-8			5	15	mV
	Input Bias Current	V_{IN} = ±50 mV_{DC}		0.1	1	µA
V_{OH}	Pin 2	V_{IN} = +125 mV_{DC} (Note 3)		8.3		V
V_{OL}	Pin 2	V_{IN} = −125 mV_{DC} (Note 3)		2.3		V
I_2, I_3	Output Current	V2 = V3 = 6.0V (Note 4)	140	180	240	µA
I_3	Leakage Current	I2 = 0, V3 = 0			0.1	µA
K	Gain Constant	(Note 3)	0.9	1.0	1.1	
	Linearity	f_{IN} = 1 kHz, 5 kHz, 10 kHz (Note 5)	−1.0	0.3	+1.0	%
OP/AMP COMPARATOR						
V_{OS}		V_{IN} = 6.0V		3	10	mV
I_{BIAS}		V_{IN} = 6.0V		50	500	nA
	Input Common-Mode Voltage		0		V_{CC}−1.5V	V
	Voltage Gain			200		V/mV
	Output Sink Current	V_C = 1.0	40	50		mA
	Output Source Current	$V_E = V_{CC}$ −2.0		10		mA
	Saturation Voltage	I_{SINK} = 5 mA		0.1	0.5	V
		I_{SINK} = 20 mA			1.0	V
		I_{SINK} = 50 mA		1.0	1.5	V
ZENER REGULATOR						
	Regulator Voltage	R_{DROP} = 470Ω		7.56		V
	Series Resistance			10.5	15	Ω
	Temperature Stability			+1		mV/°C
	Total Supply Current			3.8	6	mA

Note 1: For operation in ambient temperatures above 25°C, the device must be derated based on a 150°C maximum junction temperature and a thermal resistance of 101°C/W junction to ambient for LM2907-8 and LM2917-8, and 79°C/W junction to ambient for LM2907-14 and LM2917-14.

Note 2: Hysteresis is the sum $+V_{TH} - (-V_{TH})$, offset voltage is their difference. See test circuit.

Note 3: V_{OH} is equal to ¾ × V_{CC} − 1 V_{BE}, V_{OL} is equal to ¼ × V_{CC} − 1 V_{BE} therefore $V_{OH} - V_{OL} = V_{CC}$/2. The difference, $V_{OH} - V_{OL}$, and the mirror gain, I_2/I_3, are the two factors that cause the tachometer gain constant to vary from 1.0.

Note 4: Be sure when choosing the time constant R1 × C1 that R1 is such that the maximum anticipated output voltage at pin 3 can be reached with I_3 × R1. The maximum value for R1 is limited by the output resistance of pin 3 which is greater than 10 MΩ typically.
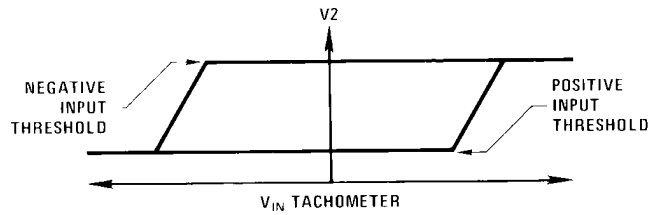
Note 5: Nonlinearity is defined as the deviation of V_{OUT} (@ pin 3) for f_{IN} = 5 kHz from a straight line defined by the V_{OUT} @ 1 kHz and V_{OUT} @ 10 kHz. C1 = 1000 pF, R1 = 68k and C2 = 0.22 mFd.
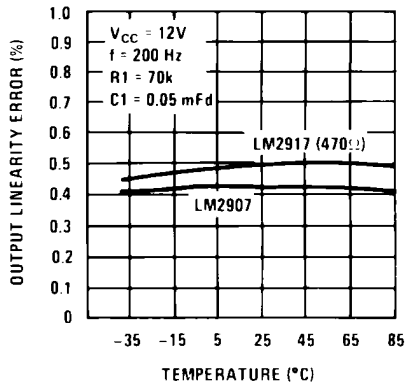
Test Circuit and Waveform
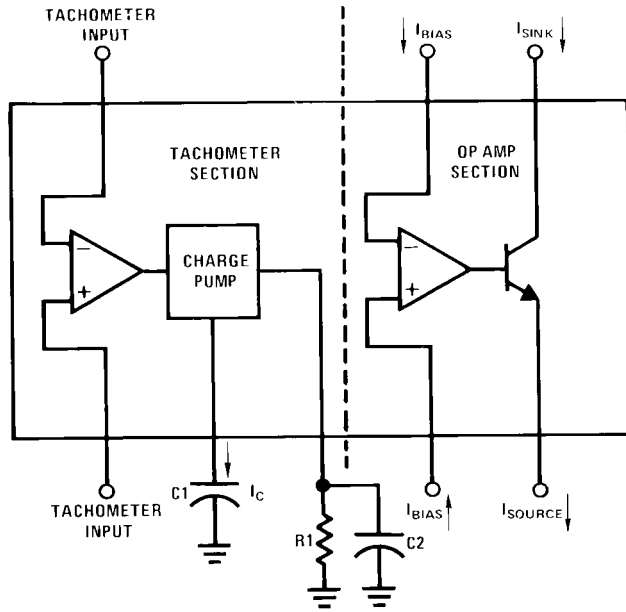
794206

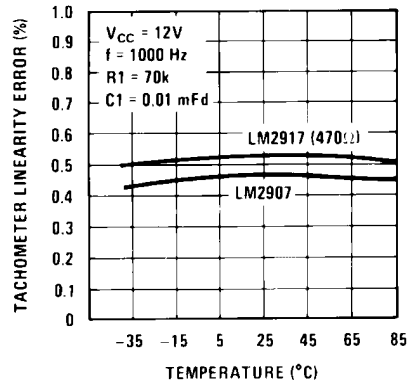**Tachometer Input Threshold Measurement**

794207

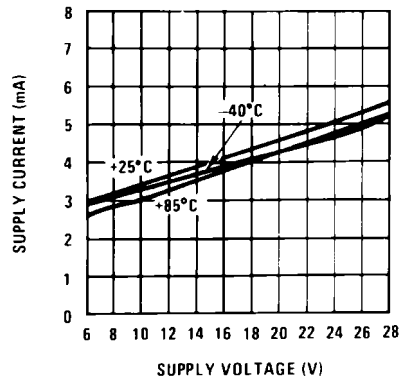# Typical Performance Characteristics

Tachometer Linearity vs Temperature

V_{CC} = 12V
f = 200 Hz
R1 = 70k
C1 = 0.05 mFd

LM2917 (470Ω)

LM2907

OUTPUT LINEARITY ERROR (%)

TEMPERATURE (°C)

794246

Tachometer Linearity vs Temperature

V_{CC} = 12V
f = 1000 Hz
R1 = 70k
C1 = 0.01 mFd

LM2917 (470Ω)

LM2907

TACHOMETER LINEARITY ERROR (%)

TEMPERATURE (°C)

794247

Total Supply Current

−40°C

+25°C

+85°C

SUPPLY CURRENT (mA)

SUPPLY VOLTAGE (V)

794240

Zener Voltage vs Temperature

V_{CC} = 12V

470Ω

860Ω

1000Ω

ZENER VOLTAGE (V)
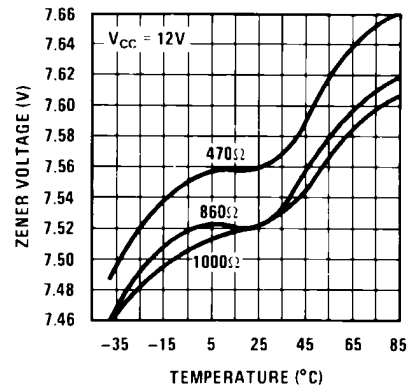
TEMPERATURE (°C)

794241

Normalized Tachometer Output (K) vs Temperature

FREQUENCY = 1000 Hz

LM2907

LM2917 (470Ω)

NORMALIZED TACHOMETER OUTPUT (K)
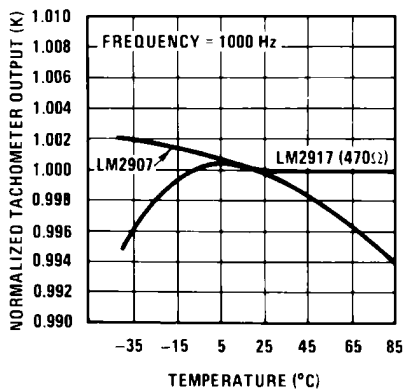
TEMPERATURE (°C)

794242

Normalized Tachometer Output (K) vs Temperature

FREQUENCY = 200 Hz

LM2907

LM2917 (470Ω)

NORMALIZED TACHOMETER OUTPUT (K)
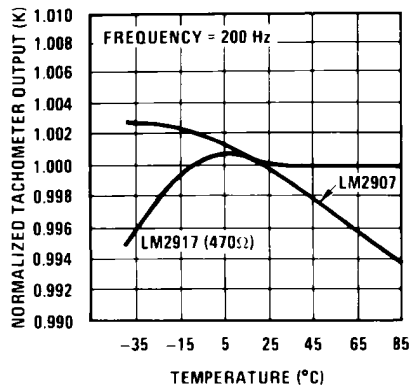
TEMPERATURE (°C)

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Tachometer Currents I₂ and I₃ vs Supply Voltage
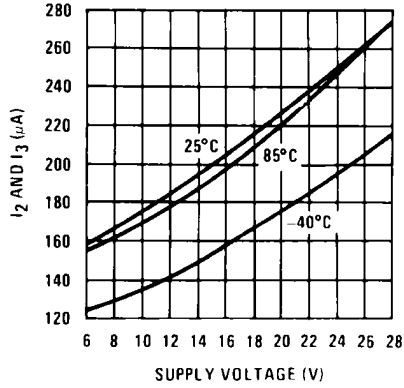
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Tachometer Currents I₂ and I₃ vs Temperature
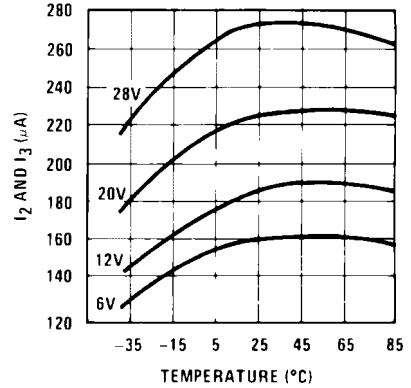
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Tachometer Linearity vs R1
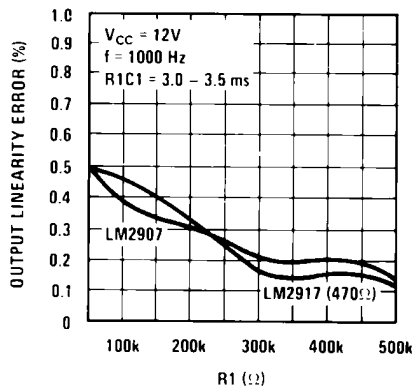
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Tachometer Input Hysteresis vs Temperature
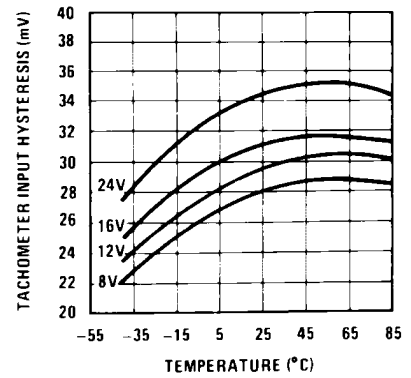
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Op Amp Output Transistor Characteristics
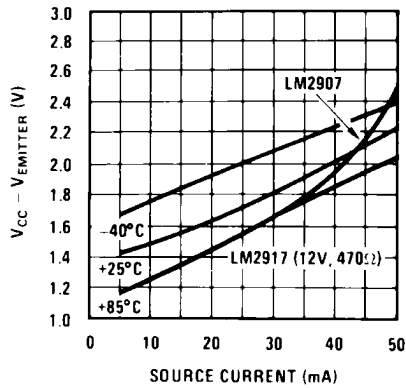
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Op Amp Output Transistor Characteristics
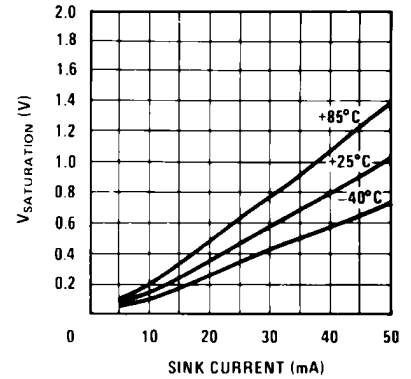
794251

Applications Information

The LM2907 series of tachometer circuits is designed for minimum external part count applications and maximum versatility. In order to fully exploit its features and advantages let's examine its theory of operation. The first stage of operation is a differential amplifier driving a positive feedback flip-flop circuit. The input threshold voltage is the amount of differential input voltage at which the output of this stage changes state. Two options (LM2907-8, LM2917-8) have one input internally grounded so that an input signal must swing above and below ground and exceed the input thresholds to produce an output. This is offered specifically for magnetic variable reluctance pickups which typically provide a single-ended ac output. This single input is also fully protected against voltage swings to ±28V, which are easily attained with these types of pickups.

The differential input options (LM2907, LM2917) give the user the option of setting his own input switching level and still have the hysteresis around that level for excellent noise rejection in any application. Of course in order to allow the inputs to attain common-mode voltages above ground, input protection is removed and neither input should be taken outside the limits of the supply voltage being used. It is very important that an input not go below ground without some resistance in its lead to limit the current that will then flow in the epi-substrate diode.

Following the input stage is the charge pump where the input frequency is converted to a dc voltage. To do this requires one timing capacitor, one output resistor, and an integrating or filter capacitor. When the input stage changes state (due to a suitable zero crossing or differential voltage on the input) the timing capacitor is either charged or discharged linearly between two voltages whose difference is $V_{CC}/2$. Then in one half cycle of the input frequency or a time equal to $1/2\ f_{IN}$ the change in charge on the timing capacitor is equal to $V_{CC}/2 \times C1$. The average amount of current pumped into or out of the capacitor then is:

$$\frac{\Delta Q}{T} = i_{c(AVG)} = C1 \times \frac{V_{CC}}{2} \times (2f_{IN}) = V_{CC} \times f_{IN} \times C1$$

The output circuit mirrors this current very accurately into the load resistor R1, connected to ground, such that if the pulses of current are integrated with a filter capacitor, then $V_O = i_c \times R1$, and the total conversion equation becomes:

$$V_O = V_{CC} \times f_{IN} \times C1 \times R1 \times K$$

Where K is the gain constant—typically 1.0.

The size of C2 is dependent only on the amount of ripple voltage allowable and the required response time.

CHOOSING R1 AND C1

There are some limitations on the choice of R1 and C1 which should be considered for optimum performance. The timing capacitor also provides internal compensation for the charge pump and should be kept larger than 500 pF for very accurate operation. Smaller values can cause an error current on R1, especially at low temperatures. Several considerations must be met when choosing R1. The output current at pin 3 is internally fixed and therefore $V_O/R1$ must be less than or equal to this value. If R1 is too large, it can become a significant fraction of the output impedance at pin 3 which degrades linearity. Also output ripple voltage must be considered and the size of C2 is affected by R1. An expression that describes the ripple content on pin 3 for a single R1C2 combination is:

$$V_{RIPPLE} = \frac{V_{CC}}{2} \times \frac{C1}{C2} \times \left(1 - \frac{V_{CC} \times f_{IN} \times C1}{I_2}\right) pk-pk$$

It appears R1 can be chosen independent of ripple, however response time, or the time it takes V_{OUT} to stabilize at a new voltage increases as the size of C2 increases, so a compromise between ripple, response time, and linearity must be chosen carefully.

As a final consideration, the maximum attainable input frequency is determined by V_{CC}, C1 and I_2:
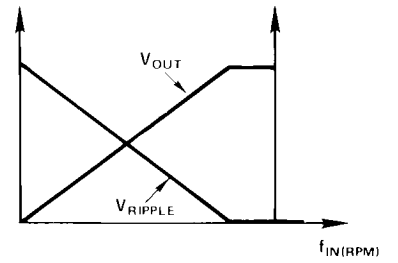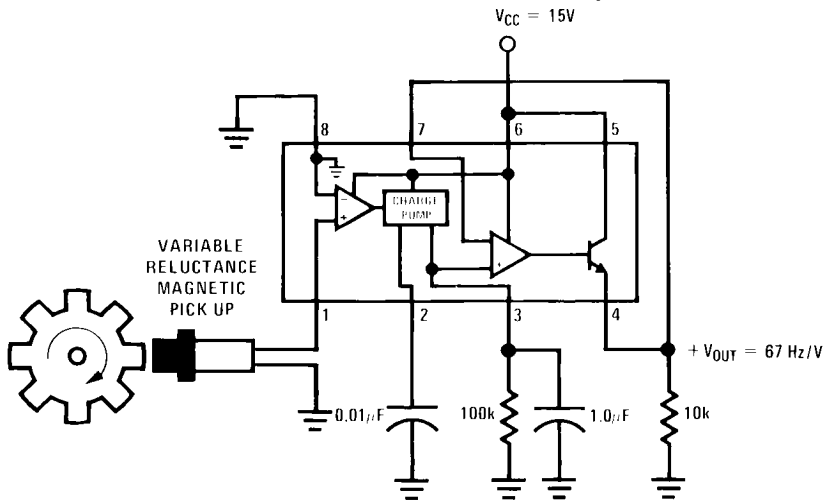
$$f_{MAX} = \frac{I_2}{C1 \times V_{CC}}$$

USING ZENER REGULATED OPTIONS (LM2917)

For those applications where an output voltage or current must be obtained independent of supply voltage variations, the LM2917 is offered. The most important consideration in choosing a dropping resistor from the unregulated supply to the device is that the tachometer and op amp circuitry alone require about 3 mA at the voltage level provided by the zener. At low supply voltages there must be some current flowing in the resistor above the 3 mA circuit current to operate the regulator. As an example, if the raw supply varies from 9V to 16V, a resistance of 470Ω will minimize the zener voltage variation to 160 mV. If the resistance goes under 400Ω or over 600Ω the zener variation quickly rises above 200 mV for the same input variation.
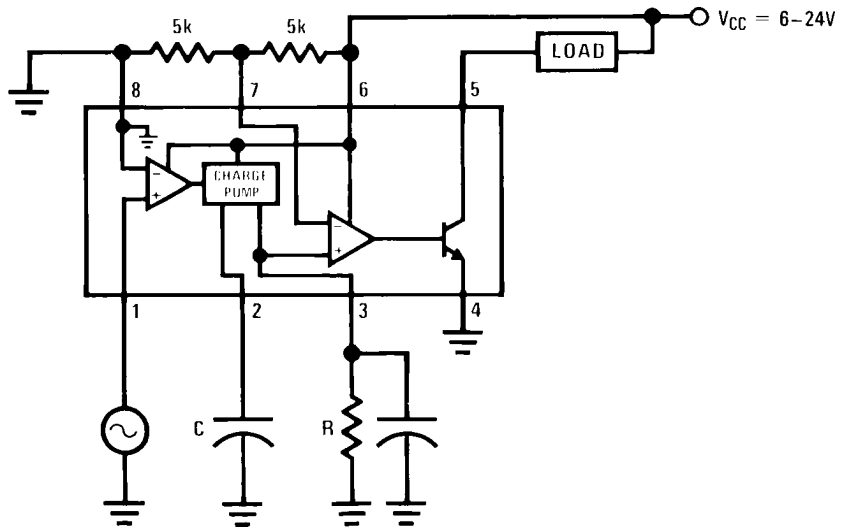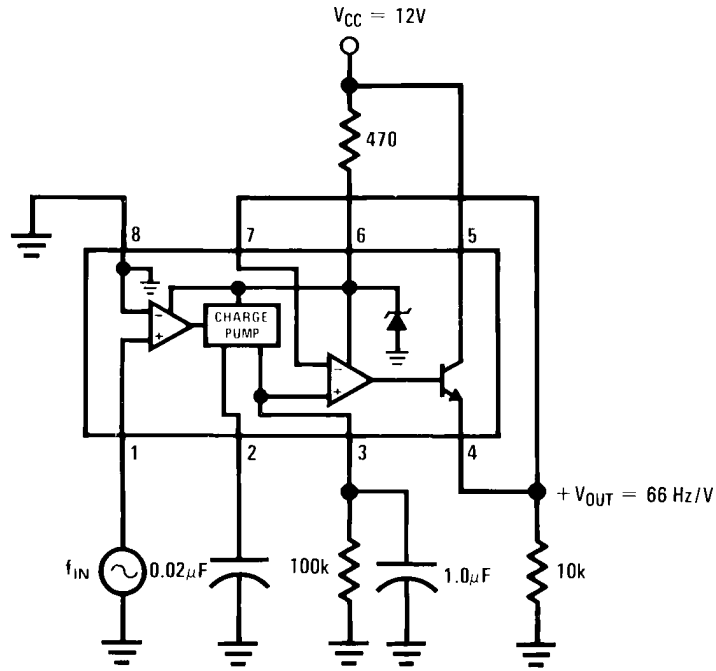
Typical Applications

Minimum Component Tachometer

$V_{CC} = 15V$

VARIABLE
RELUCTANCE
MAGNETIC
PICK UP

$0.01\mu F$ 100k $1.0\mu F$ 10k

$+ V_{OUT} = 67$ Hz/V

V_{OUT}

V_{RIPPLE}

$f_{IN(RPM)}$

794208

"Speed Switch", Load is Energized when $f_{IN} \geq (1 / (2RC))$

5k 5k LOAD $V_{CC} = 6{-}24V$

CHARGE PUMP

C R

794209

Zener Regulated Frequency to Voltage Converter

$V_{CC} = 12V$

470

8 7 6 5

CHARGE PUMP

1 2 3 4

f_{IN} $0.02\mu F$ 100k $1.0\mu F$ 10k

$+ V_{OUT} = 66\,Hz/V$

794210

Breaker Point Dwell Meter

B+

10k 5k 5k 470

11 12 10 9 8

CHARGE PUMP

POINTS

GROUND 10k

1 2 3 4 5

20k $0.02\mu F$ 100k 1000 pF
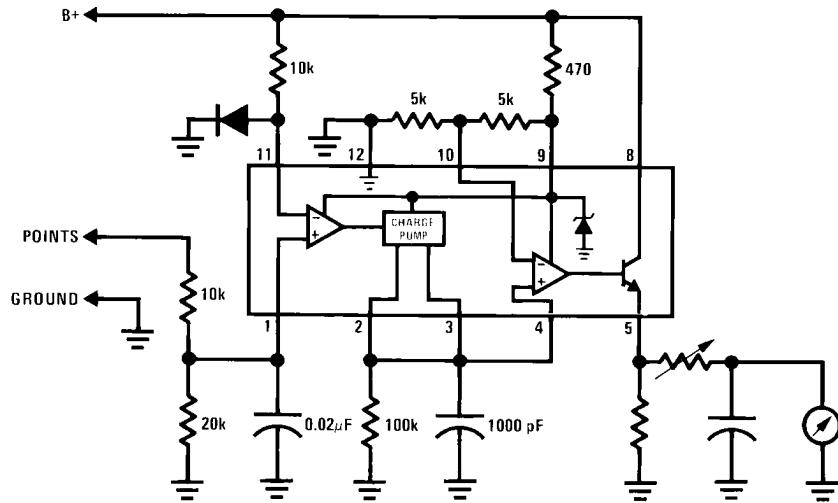
794211

Voltage Driven Meter Indicating Engine RPM
V_O = 6V @ 400 Hz or 6000 ERPM (8 Cylinder Engine)
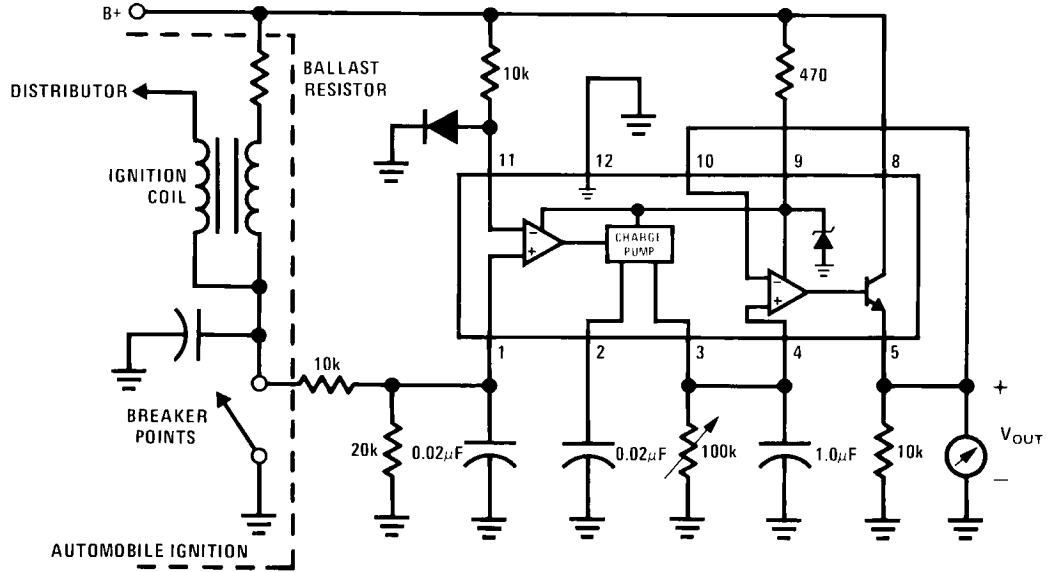
794212

Current Driven Meter Indicating Engine RPM
I_O = 10 mA @ 300 Hz or 6000 ERPM (6 Cylinder Engine)
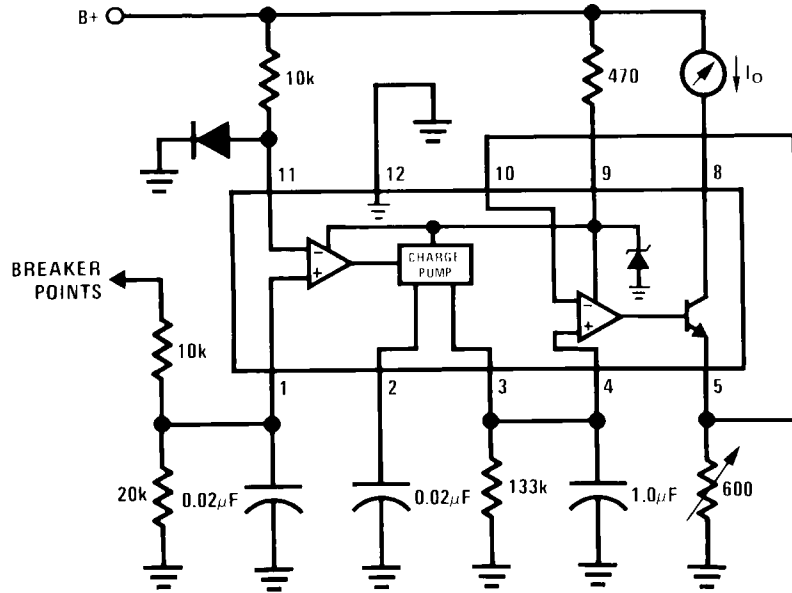
794213

Capacitance Meter
$V_{OUT} = 1V–10V$ for $C_X = 0.01$ to 0.1 mFd
(R = 111k)
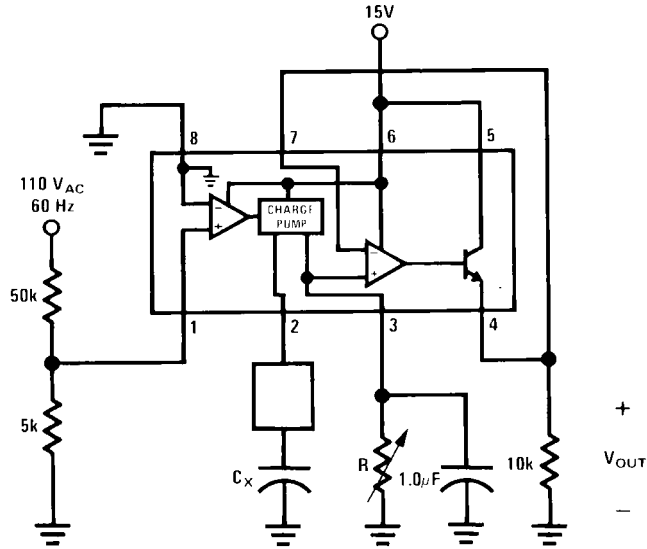
794214

Two-Wire Remote Speed Switch
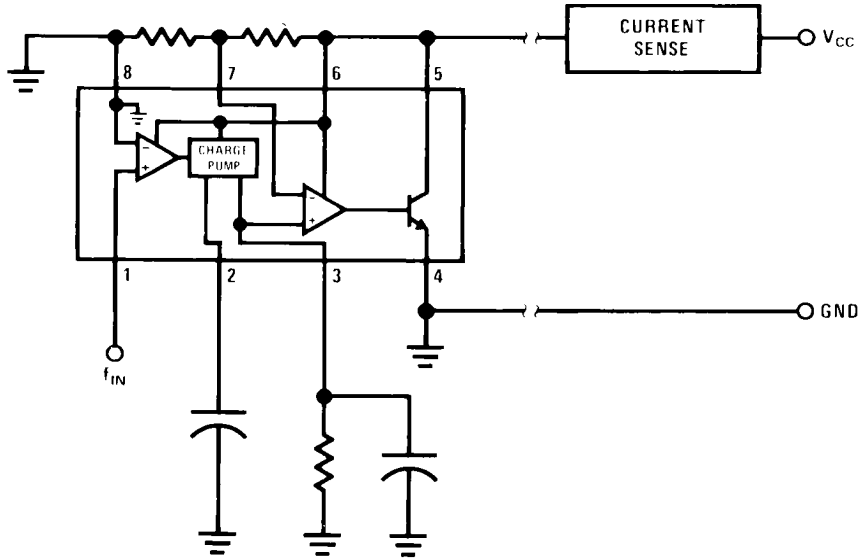
794215

100 Cycle Delay Switch
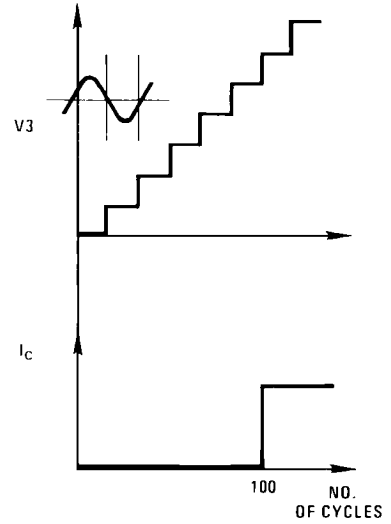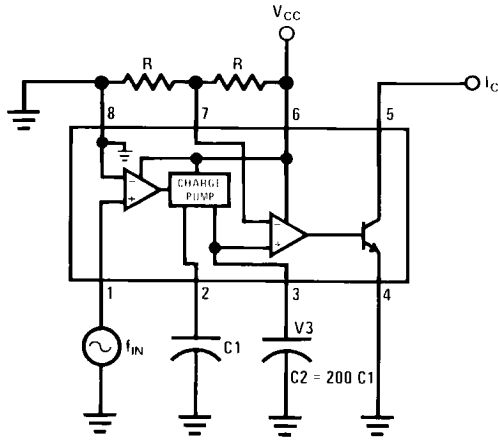
794216

V3 steps up in voltage by the amount $\dfrac{V_{CC} \times C1}{C2}$

for each complete input cycle (2 zero crossings)

Example:
if C2 = 200 C1 after 100 consecutive input cycles.

$$V3 = 1/2 \ V_{CC}$$

Variable Reluctance Magnetic Pickup Buffer Circuits
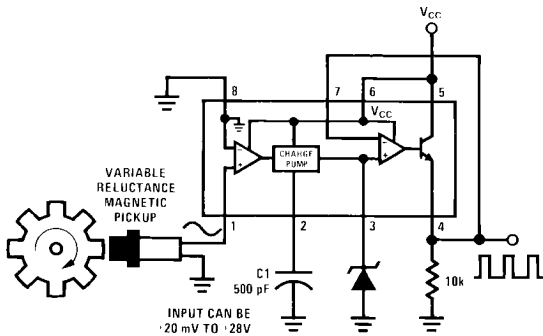
794239

Precision two-shot output frequency
equals twice input frequency.

$$\text{Pulse width} = \frac{V_{CC}}{2} \cdot \frac{C1}{I2}$$

Pulse height = V_{ZENER}
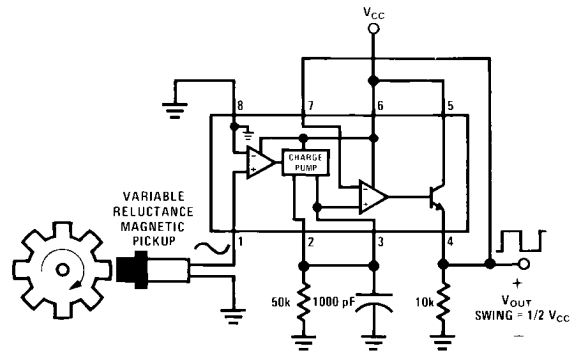
794217

Finger Touch or Contact Switch
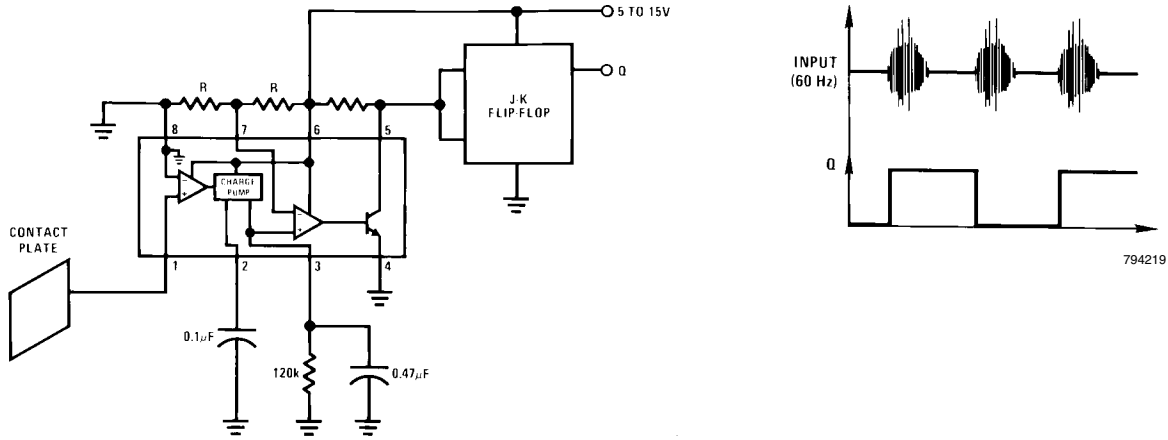
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Flashing LED Indicates Overspeed
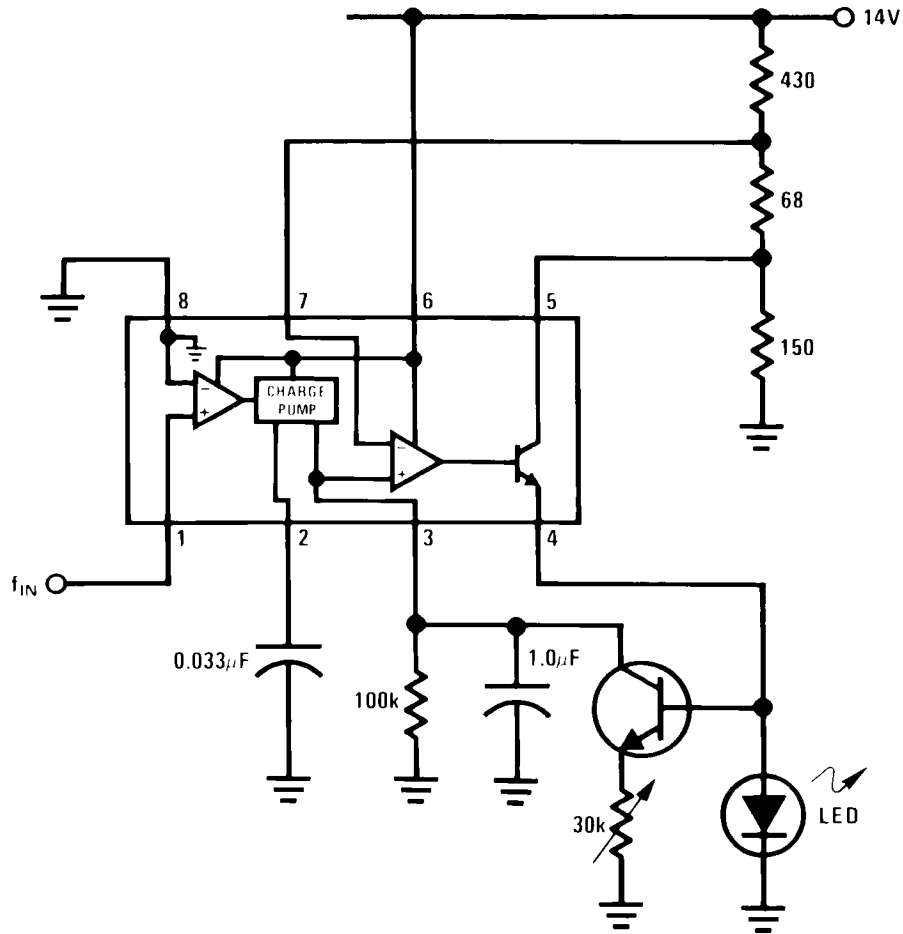
794220

Flashing begins when f$_{IN}$ ≥ 100 Hz.
Flash rate increases with input frequency
increase beyond trip point.

Frequency to Voltage Converter with 2 Pole Butterworth Filter to Reduce Ripple

V_CC

11 12 10 9 8

CHARGE PUMP

f_IN

1 2 3 4 5

R

R

C

0.05μF 100k 2C 10k V_OUT + −
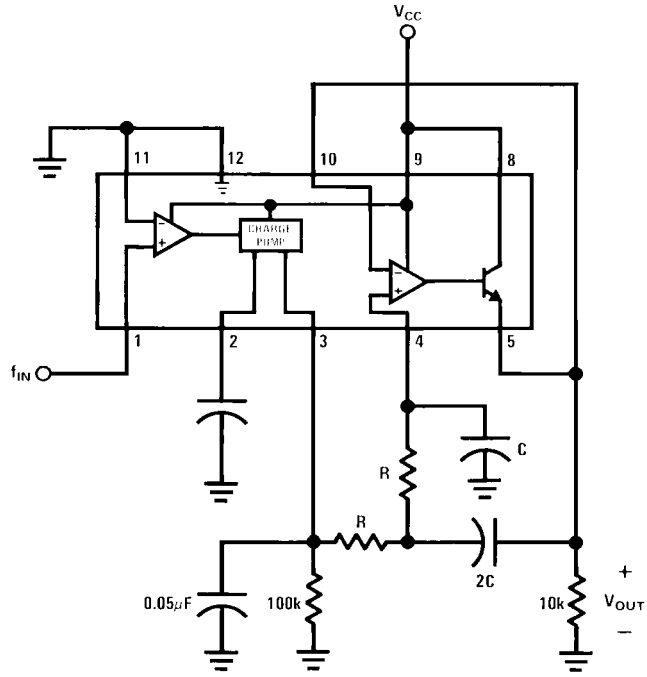
794221

$$f_{POLE} = \frac{0.707}{2\pi RC}$$

$$\tau_{RESPONSE} = \frac{2.57}{2\pi f_{POLE}}$$

Overspeed Latch

V_CC

R2 R1 470

8 7 6 5

CHARGE PUMP

1 2 3 4

f_IN C R V_OUT + −

794222

V_OUT

f_IN
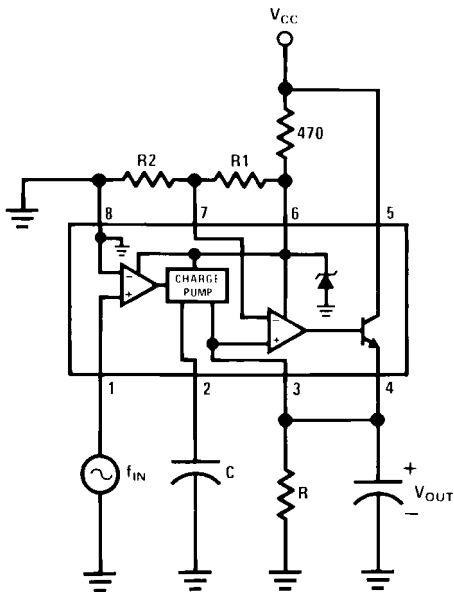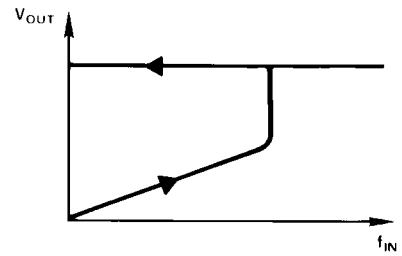
794223

Output latches when

$$f_{IN} = \frac{R2}{R1 + R2} \frac{1}{RC}$$

Reset by removing V_CC.

Some Frequency Switch Applications May Require Hysteresis in the Comparator Function Which can be Implemented in Several Ways
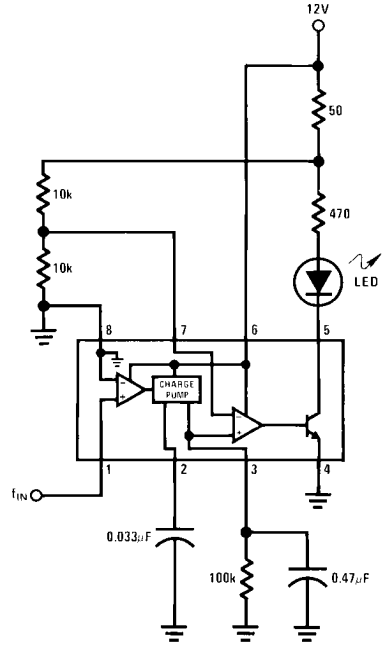
794224

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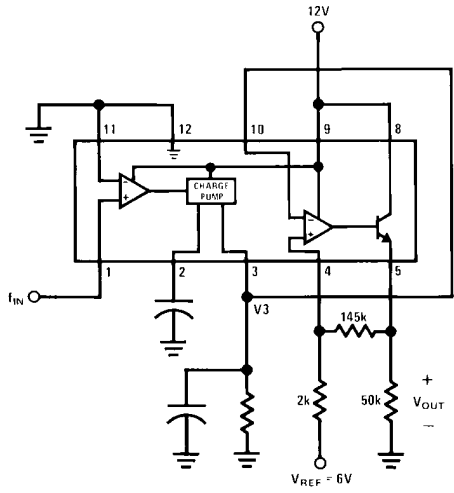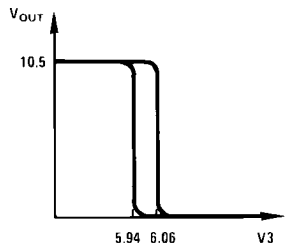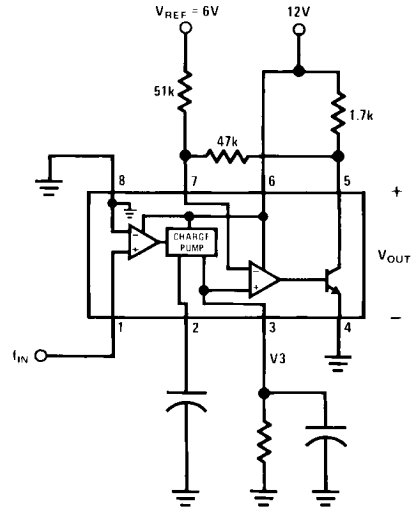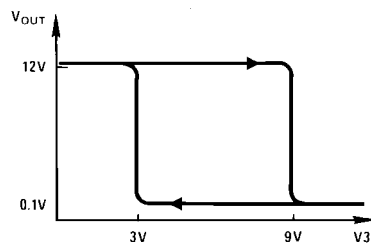
Changing the Output Voltage for an Input Frequency of Zero
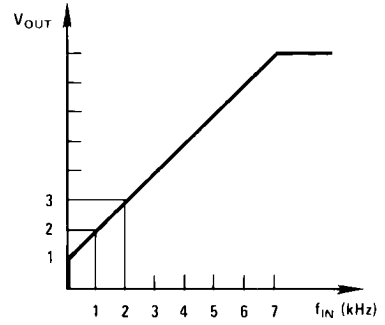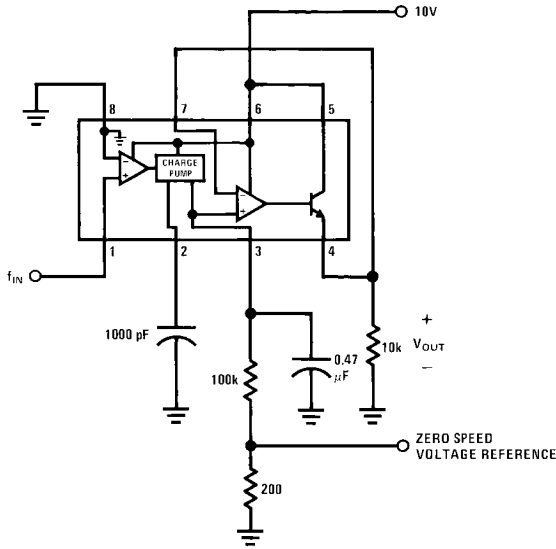
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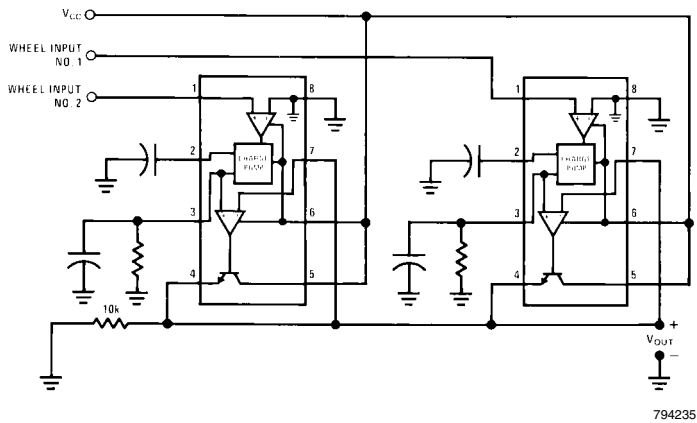**Changing Tachometer Gain Curve or Clamping the Minimum Output Voltage**
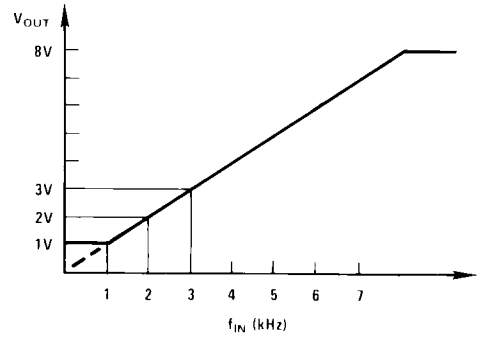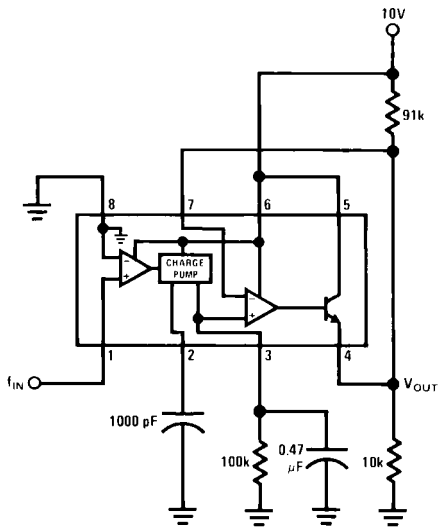
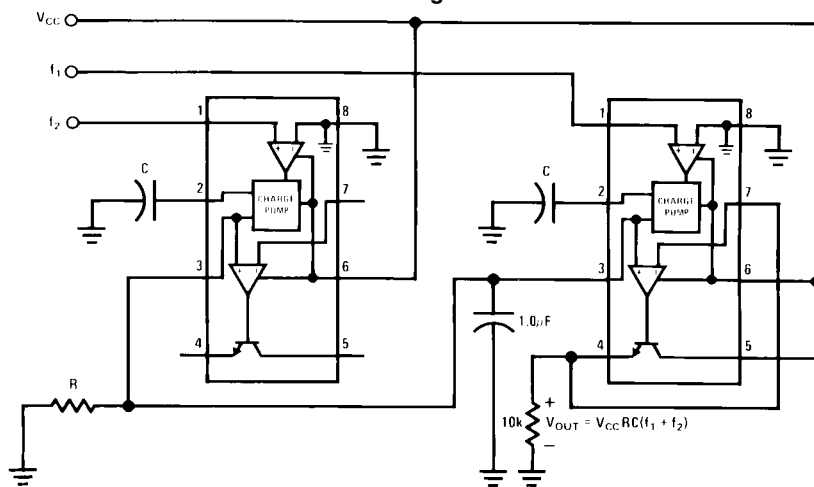
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Anti-Skid Circuit Functions

"Select-Low" Circuit
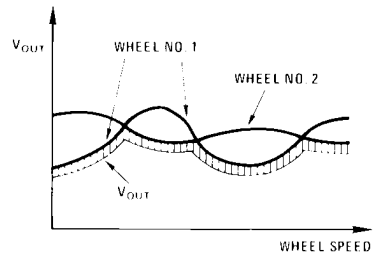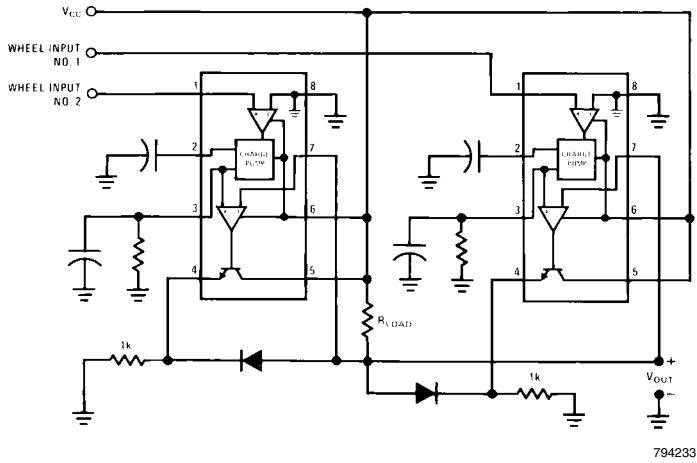
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V_{OUT} is proportional to the lower of the two input wheel speeds.

"Select-High" Circuit
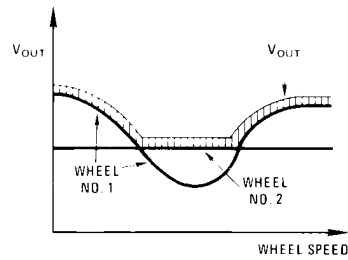
794235

794236

V_{OUT} is proportional to the higher of the two input wheel speeds.
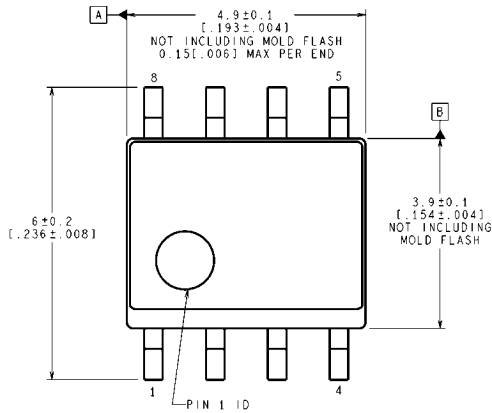
"Select-Average" Circuit

$$V_{OUT} = V_{CC} RC(f_1 + f_2)$$

794237

Equivalent Schematic Diagram
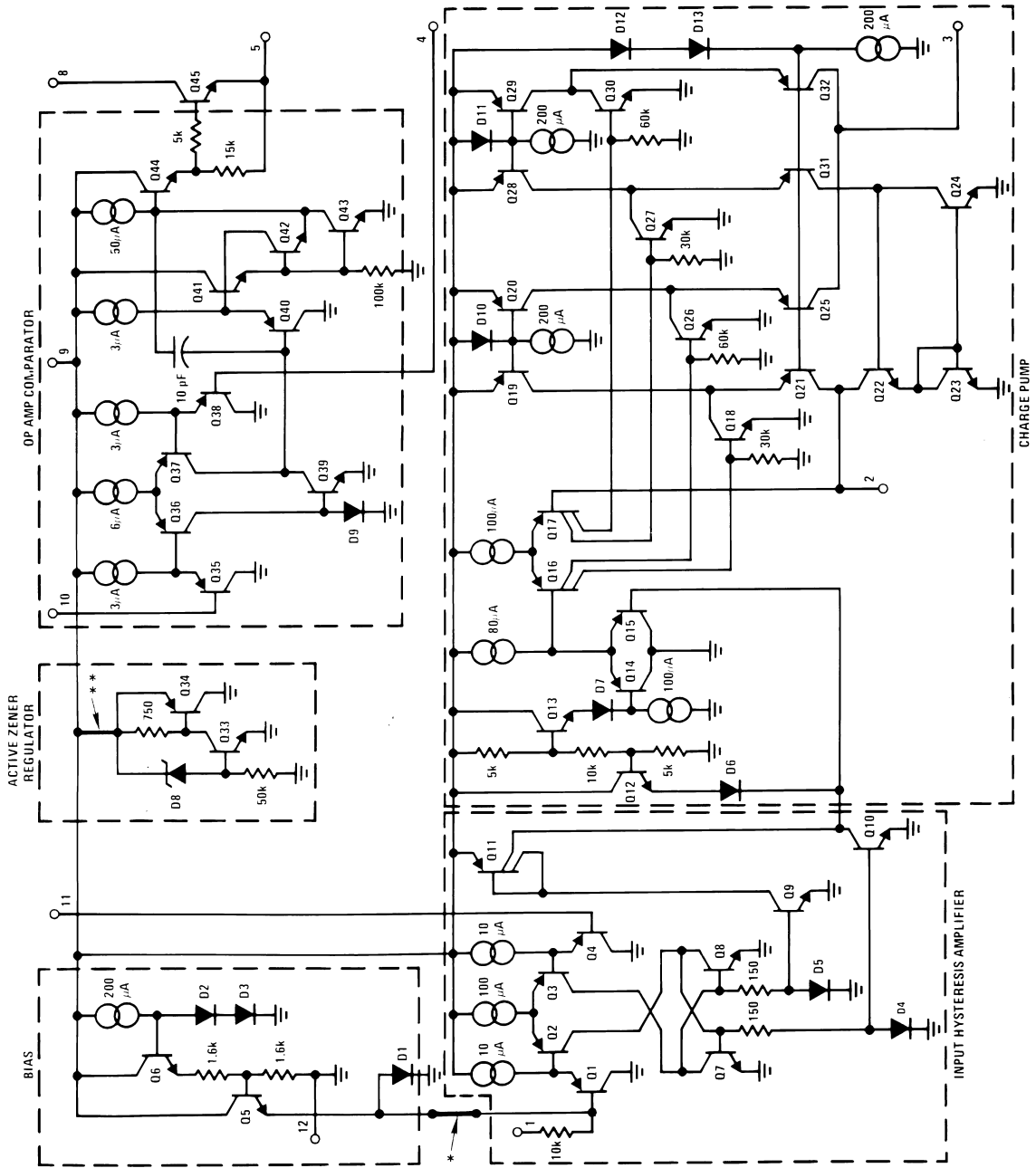
794238

*This connection made on LM2907-8 and LM2917-8 only.
**This connection made on LM2917 and LM2917-8 only.

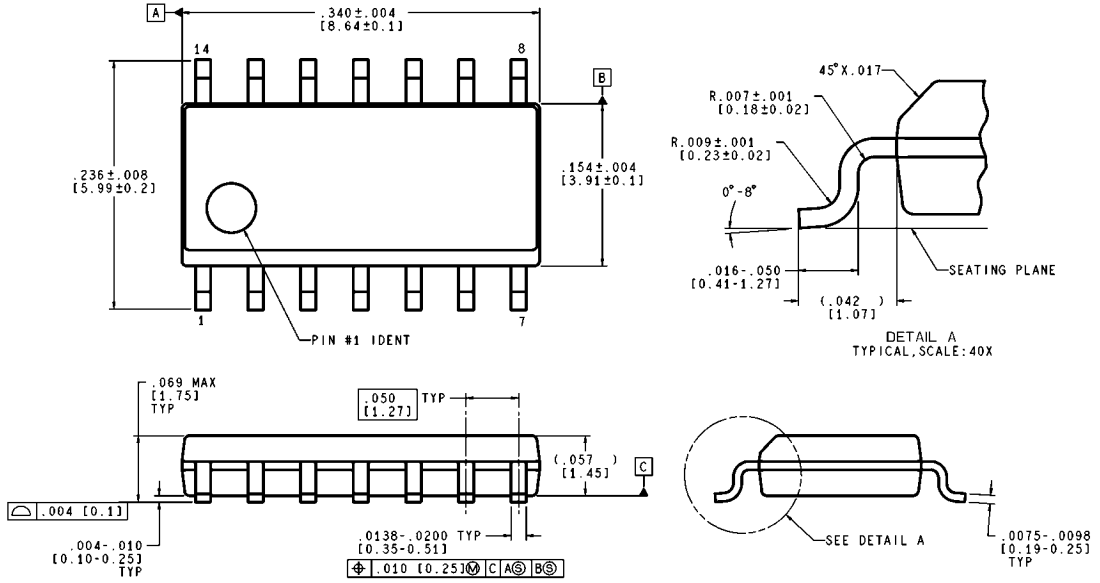# Physical Dimensions inches (millimeters) unless otherwise noted

4.9±0.1
[.193±.004]
NOT INCLUDING MOLD FLASH
0.15[.006] MAX PER END

6±0.2
[.236±.008]

3.9±0.1
[.154±.004]
NOT INCLUDING
MOLD FLASH

PIN 1 ID

8X (0.6)
[.02]

8X (2.2)
[.09]

(5.2)
[.20]

6X (1.27)
[.05]

RECOMMENDED LAND PATTERN

1.35-1.75
[.053-.069]
TYP

6X 1.27
[.050]

(1.45)
[.057]

8X 0.35-0.51
[.0138-.0200]

0.10-0.25
[.004-.010]
TYP

R0.18±0.02
[.007±.0008]

R0.23±0.02
[.009±.0008]

0.25
[.010]
GAGE PLANE

0°-8°

45° X 0.25-0.50
[.010-.020]

SEATING
PLANE

0.41-1.27
[.016-.050]

(1.04)
[.041]

0.190-0.248
[.0075-.0098]
TYP
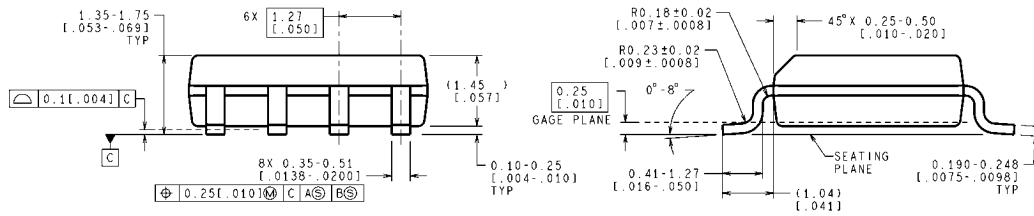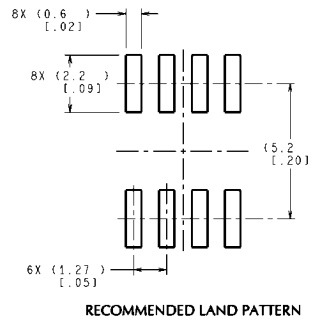
CONTROLLING DIMENSION IS MILLIMETER
VALUES IN [ ] ARE INCHES
DIMENSIONS IN ( ) FOR REFERENCE ONLY

M08A (Rev L)

**8-Lead (0.150 Wide) Molded Small Outline Package, JEDEC
Order Number LM2907M-8 or LM2917M-8
NS Package Number M08A**

.340±.004
[8.64±0.1]

14   8

B

.236±.008
[5.99±0.2]

.154±.004
[3.91±0.1]

1   7

PIN #1 IDENT

45°X.017

R.007±.001
[0.18±0.02]

R.009±.001
[0.23±0.02]

0°-8°

.016-.050
[0.41-1.27]

(.042)
[1.07]

SEATING PLANE

DETAIL A
TYPICAL,SCALE:40X

.069 MAX
[1.75]
TYP

.050
[1.27]   TYP

(.057)
[1.45]   C

.004 [0.1]

.004-.010
[0.10-0.25]
TYP

.0138-.0200 TYP
[0.35-0.51]

⊕ .010 [0.25] Ⓜ C AⓈ BⓈ

SEE DETAIL A

.0075-.0098
[0.19-0.25]
TYP

CONTROLLING DIMENSION IS INCH
VALUES IN [ ] ARE MILLIMETERS

M14A (Rev J)

Molded SO Package (M)
Order Number LM2907M or LM2917M
NS Package Number M14A

0.373-0.400
(9.474-10.16)

0.090
(2.286)

0.092
(2.337)   DIA

PIN NO. 1 IDENT

OPTION 1

8   7   6   5

0.250±0.005
(6.35±0.127)

1   2   3   4

0.032±0.005
(0.813±0.127)
RAD

PIN NO. 1 IDENT

OPTION 2

8   7

1

0.280
(7.112)   MIN

0.030
(0.762)   MAX

0.300-0.320
(7.62-8.128)

0.040
(1.016)   TYP

0.039
(0.991)

0.145-0.200
(3.683-5.080)

20°±1°

0.130±0.005
(3.302±0.127)

95°±5°

0.125
(3.175)
DIA
NOM

0.065
(1.651)

0.125-0.140
(3.175-3.556)

0.020
(0.508)
MIN

90°±4°
TYP

0.009-0.015
(0.229-0.381)

0.325 +0.040
      -0.015

(8.255 +1.016)
       -0.381

0.018±0.003
(0.457±0.076)

0.100±0.010
(2.540±0.254)

0.045±0.015
(1.143±0.381)

0.060
(1.524)

0.050
(1.270)

N08E (REV F)

Molded Dual-In-Line Package (N)
Order Number LM2907N-8 or LM2917N-8
NS Package Number N08E
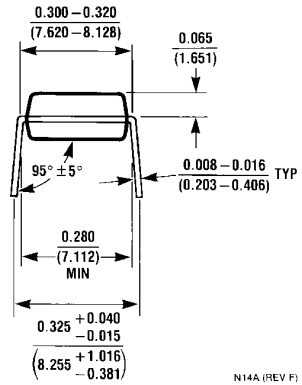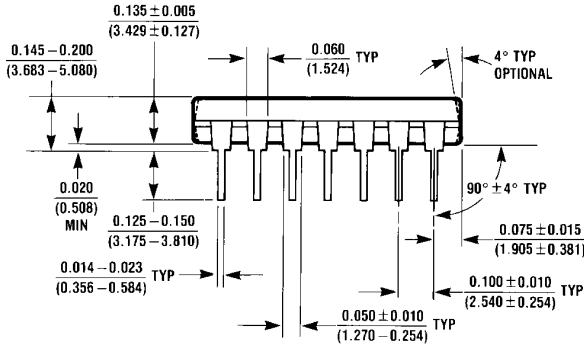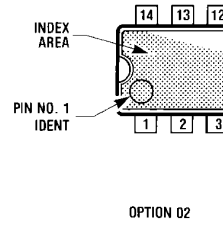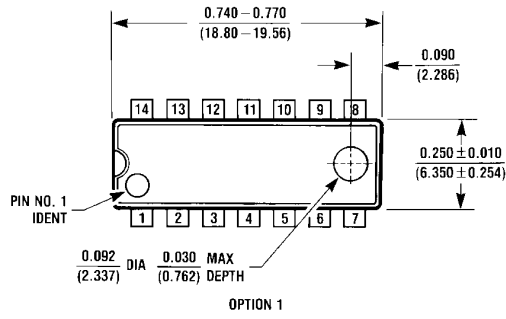
Molded Dual-In-Line Package (N)
Order Number LM2907N or LM2917N
NS Package Number N14A

Notes

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Voltage Reference	www.national.com/vref	Design Made Easy	www.national.com/easy
PowerWise® Solutions	www.national.com/powerwise	Solutions	www.national.com/solutions
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Wireless (PLL/VCO)	www.national.com/wireless	Analog University®	www.national.com/AU